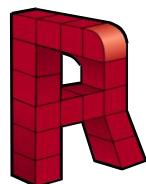




Acknowledgements

- Special thanks to:
- European Social Fund (Kess Scholarship);
- Joe Cartwright – Seismic 3D Labs, Cardiff University
- Rockfield Software Ltd.

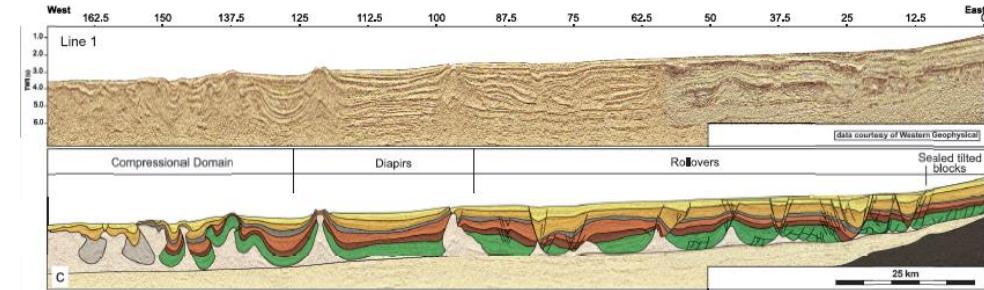


Main Goal: Determine main controls on structural styles and reservoir properties in a gravity driven system underlain by a mobile sub-strate

Structural questions:

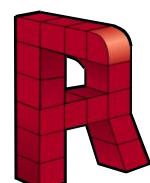
Major controls on structural style:

- timing of activity of structures (basement subsidence vs. sedimentary loading)
- spacing and style of extensional rafts
- transition to compressional regime
- influence of basement geometry



Rationale

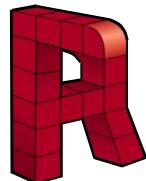
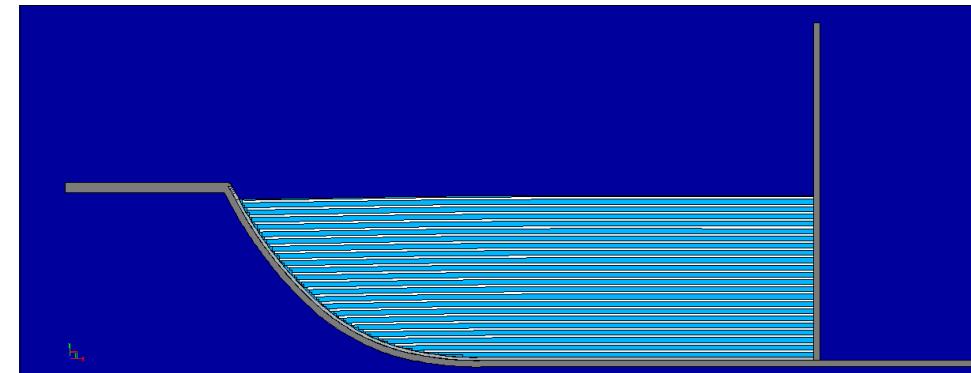
- Fort et al, 2004 performed laboratory experiments on brittle-ductile models to study thin-skinned deformation above the salt at margin scale
- The experiments are designed with the salt basin wedging out, both landward and seaward, and entirely covered by sediments at the onset of gravity driven deformation.
- They show that the experiments capture the main mechanisms observed in the seismic images



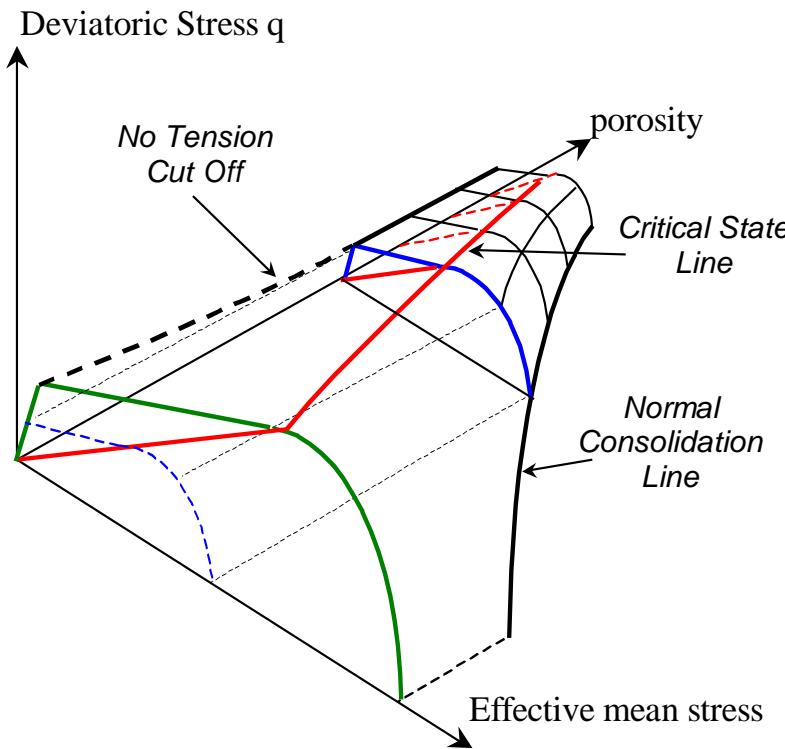


ELFEN – Modelling Approach

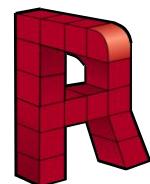
- Finite Element Method
- Physics based approach incorporating large strain
- Enhanced rheological models (constitutive models) for rocks and salt
- Enhanced fault and localisation prediction
- Includes Sedimentation and Erosion



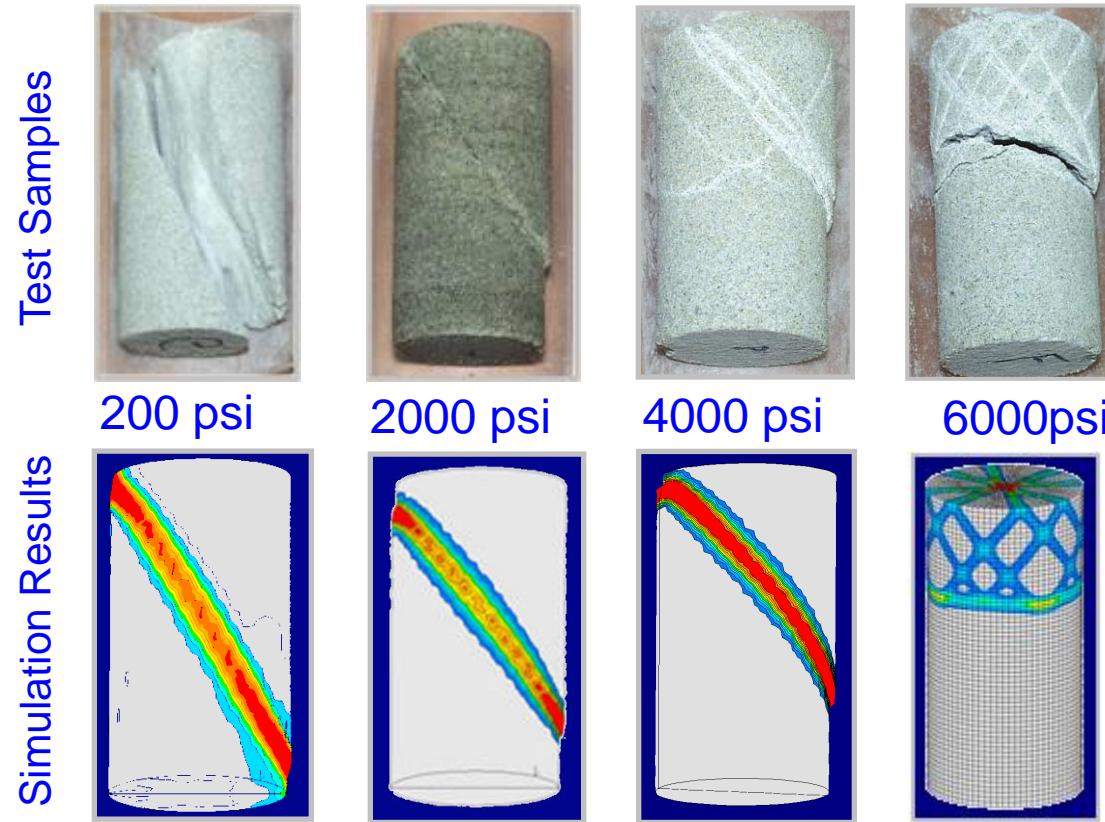
Rockfield's SR3 Constitutive Model



- State Boundary Surface Based on Critical State Theory.
- Represents Increased strength due to Mechanical Compaction and Strength Reduction due to Shear Failure
- Fracture Mechanics Concepts facilitate scale-up from experimental to field scale
- Localisation Identification Algorithms enable the prediction of the formation and evolution of new faults



Dependence of fracture angle on confining pressure





Regional-Scale Salt Tectonics Modelling

Constitutive Model for the Sand

SR3 Model - Characterisation

- The constitutive model has been shown to provide a good prediction of the response in sandbox tests in a number of different stress regimes.

- Elastic Properties:**

Young's Modulus (E) = 75,000 Pa

Poisson's Ratio (ν) = 0.3

- Initial Porosity**

ϕ_0 = 0.45

- SR3 Plasticity:**

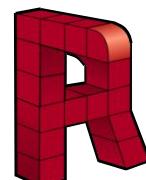
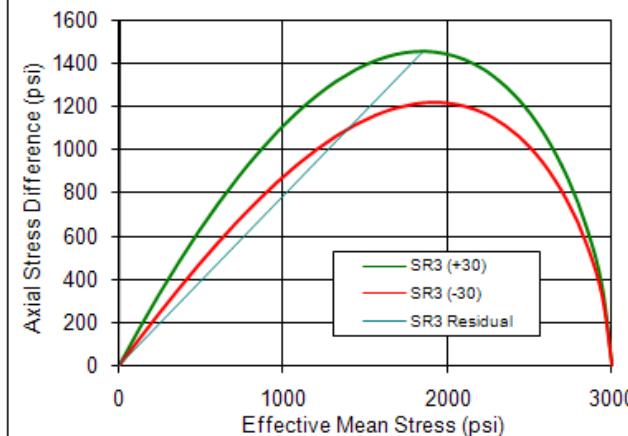
Residual Friction M = 0.79 ϕ_{cs} = 20.34°

Yield Surface Definition

Soft Rock 3 Model

Yield Surface Definition Parameters	
Pre-Consolidation Pressure p_c	3000
Friction Parameter ϕ (°)	55.00
Tensile Intercept p_t	-1.00
Exponent n	1.6
Friction Parameter ψ (°)	45.00
	0.785
Deviatoric Correction (alpha)	0.25
Beta 0	0.6
Beta 1	3.00E-04

Residual Friction Angle ϕ_{cs}	20.34
q_{cs}/p_{cs}	0.79



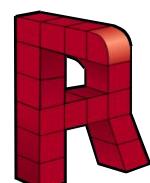
Herschel-Bulkley Model

- The silicone is represented using a Herschel-Bulkley material model. This relates the shear stress with the shear strain rate via

$$\tau = \tau_0 + k \dot{\gamma}^n$$

where τ_0 is the initial shear strength, k is the consistency parameter and n is an exponent.

- When $\tau_0 \rightarrow 0$ and $n = 1$ then this becomes a Newtonian fluid where the consistency parameter (k) is the fluid viscosity (μ)
- The silicon is defined as being Newtonian with $\mu = 10000 \text{ Pa.s}$ (2.778 Pa.hrs).
- This is achieved in ELFEN by setting
 $\tau_0 = 0.2 \text{ Pa}$
 $n = 1$
 $k = 2.778 \text{ Pa.hrs}$



Geometry

- Parametrically Defined to allow modification **slopes**, pre-kinematic sediment and salt thickness, **syn-kinematic layer thickness** and extent, sedimentation rate
- The **pre-kinematic layer is 5mm thick** in the extensional zone and may be either constant thickness or tapered towards the toe of the slope

Loading and Boundary Conditions

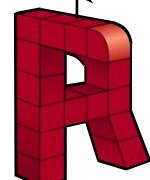
- Multi-stage analysis comprising
- Gravity initialisation of the salt and pre-kinematic sand
- Sedimentation of the syn-kinematic layers after a specified time (typically 5hrs)
- No slip at the sediment/sandbox and salt/sandbox interfaces.

Pre-kinematic Sand

Syn-kinematic Sand Layers

Salt

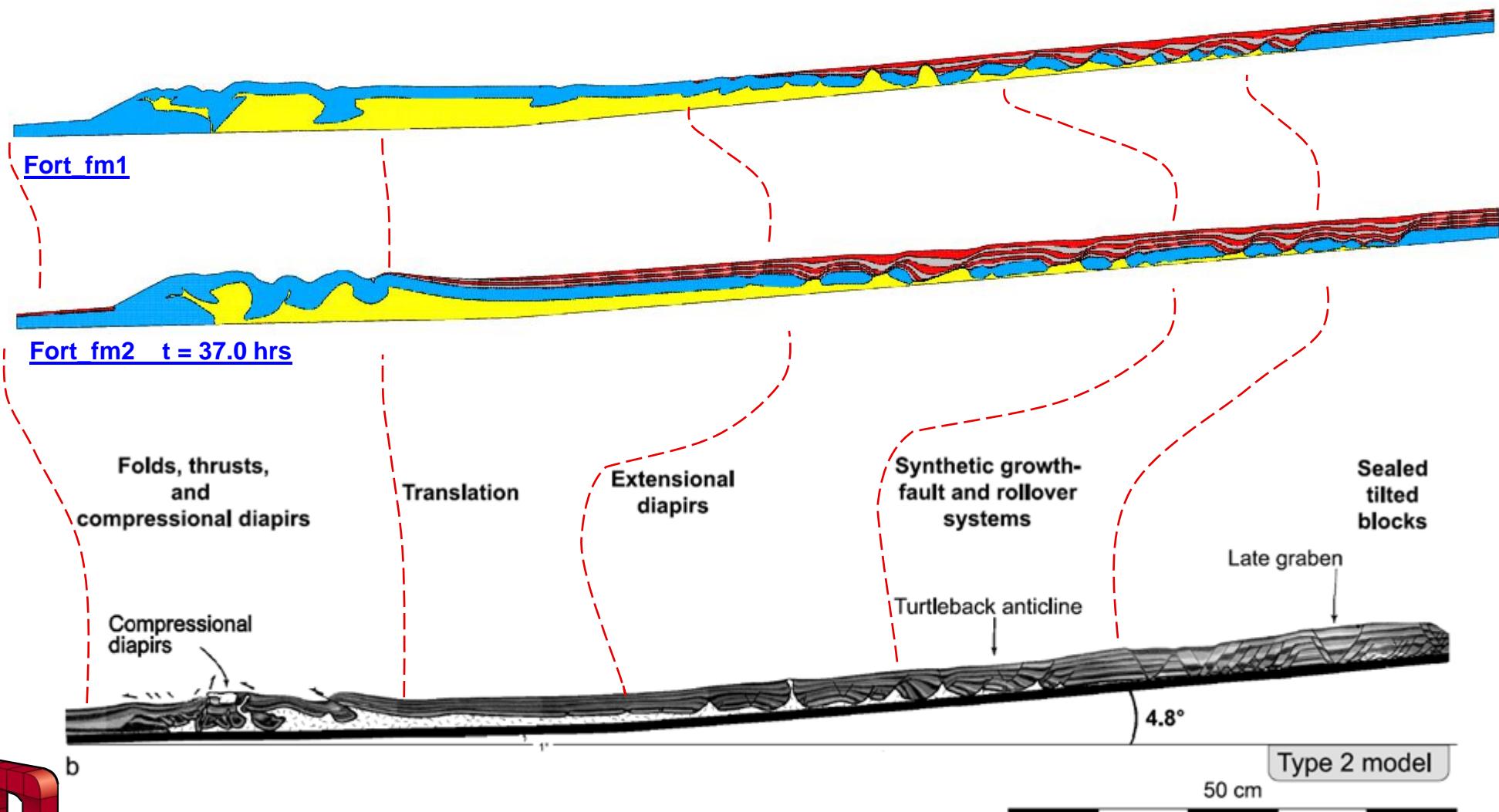
Typically 1500mm



Regional-Scale Salt Tectonics Modelling

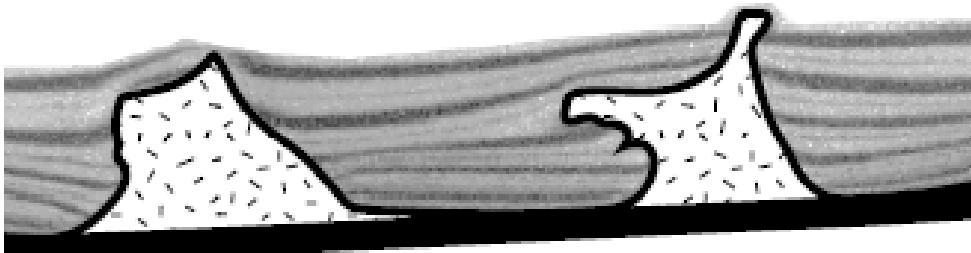
Fort et al. (2004) Models

Fort_fm1 - Distal slope angle 1°. Proximal slope angle 4.8°.
Fort_fm2 - Distal slope angle 1°. Proximal slope angle 3.8°.



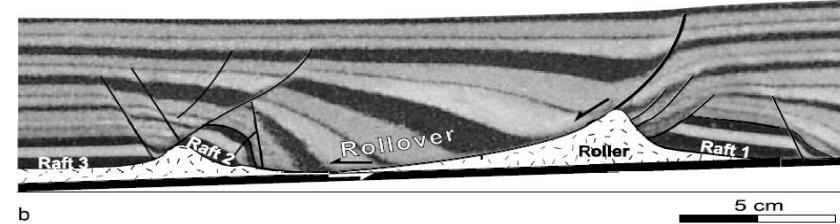
Comparison of Structural Styles

Fort_fm1



Diapirs in the proximal extension zone

Fort_fm2

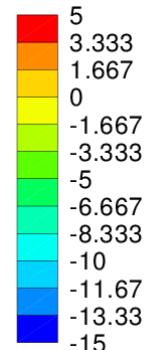
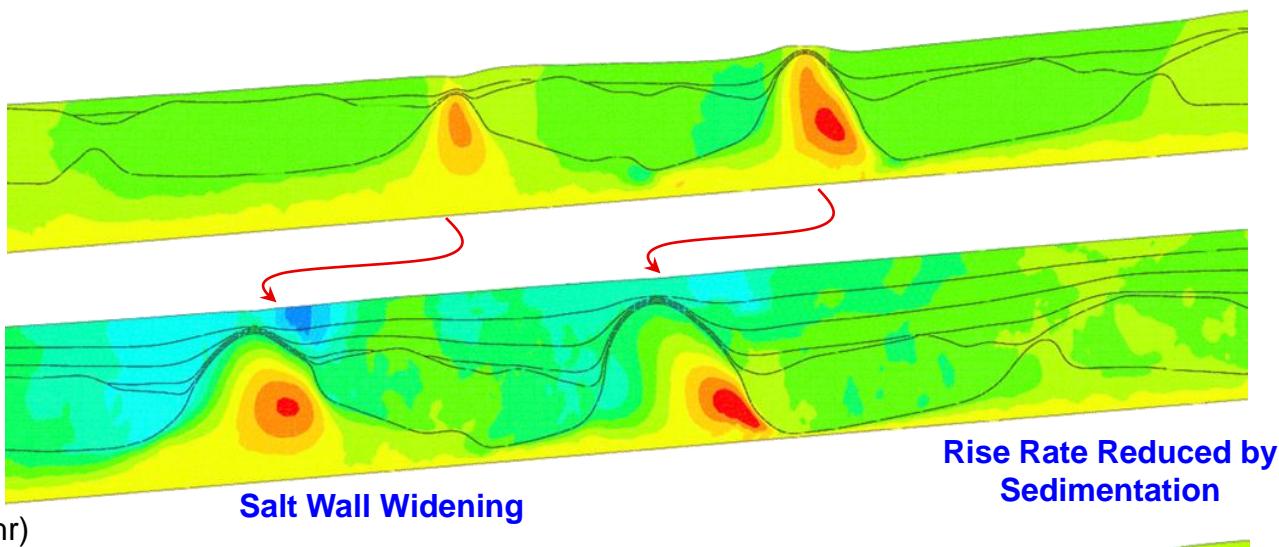


Salt rollers in the proximal extension zone

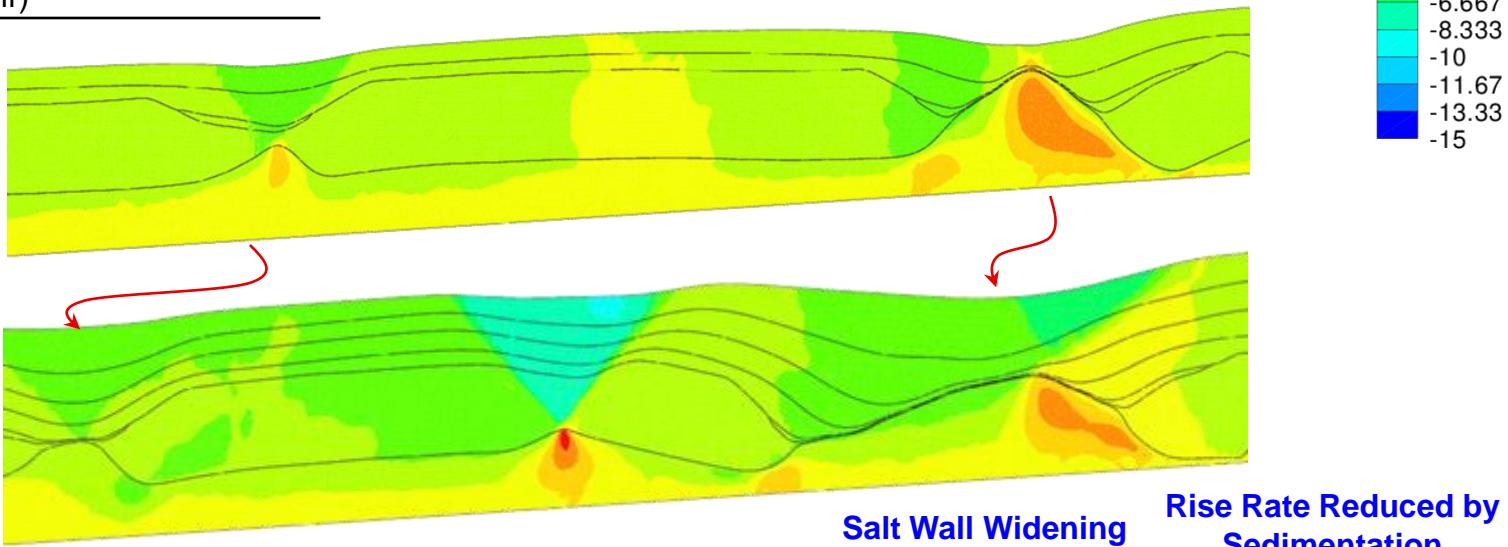
Regional-Scale Salt Tectonics Modelling

Diapiric Rise Rates

Fort_fm1



Fort_fm2



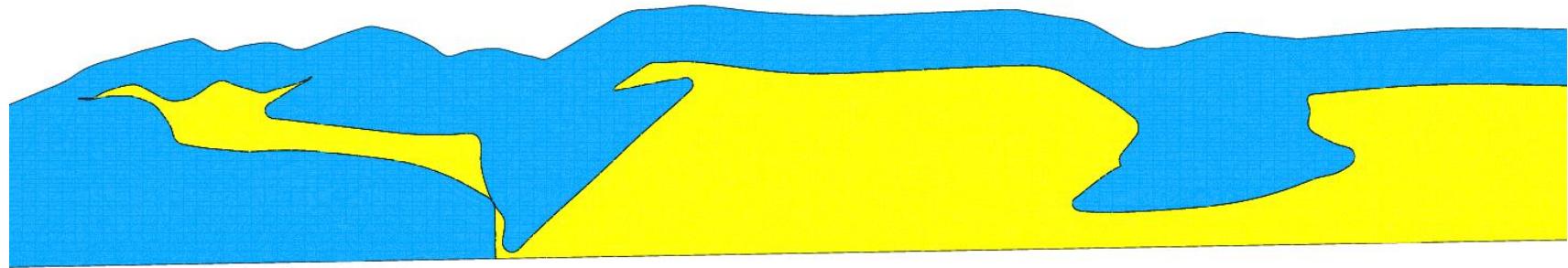
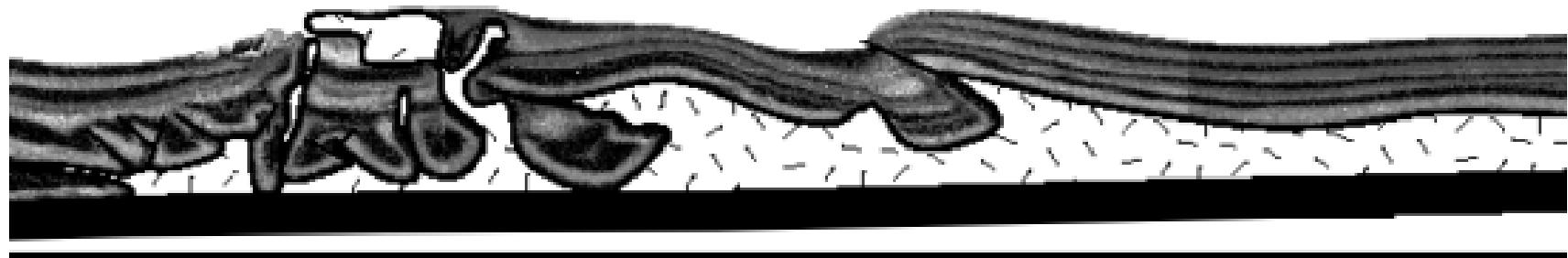
R

Rockfield

GSA – Beyond Balanced Sections 10th October 2011

Slide 12

Comparison of Structural Styles



Fort_fm1

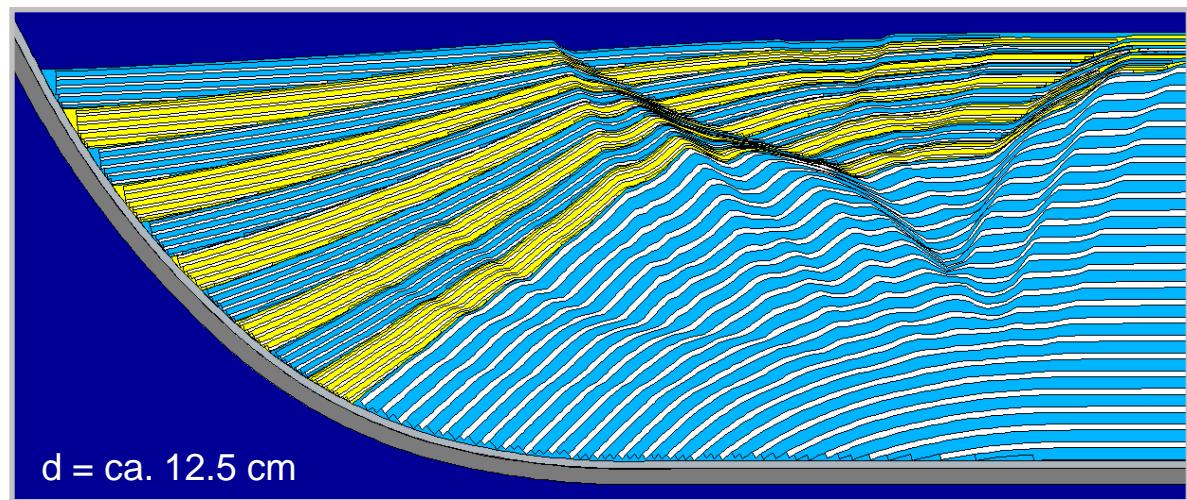
Enlarged view of compressional deformation in the physical and computational models

Regional-Scale Salt Tectonics Modelling

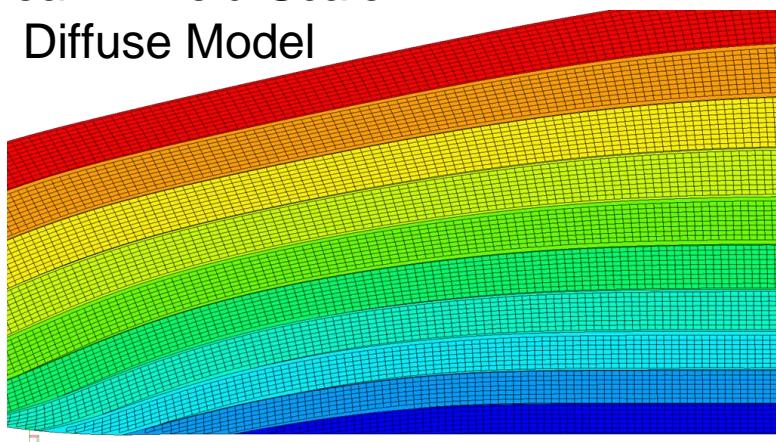
McClay E30/E37 Listric Fault Experiment and Prediction

Bench-scale Simulation

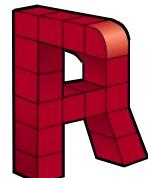
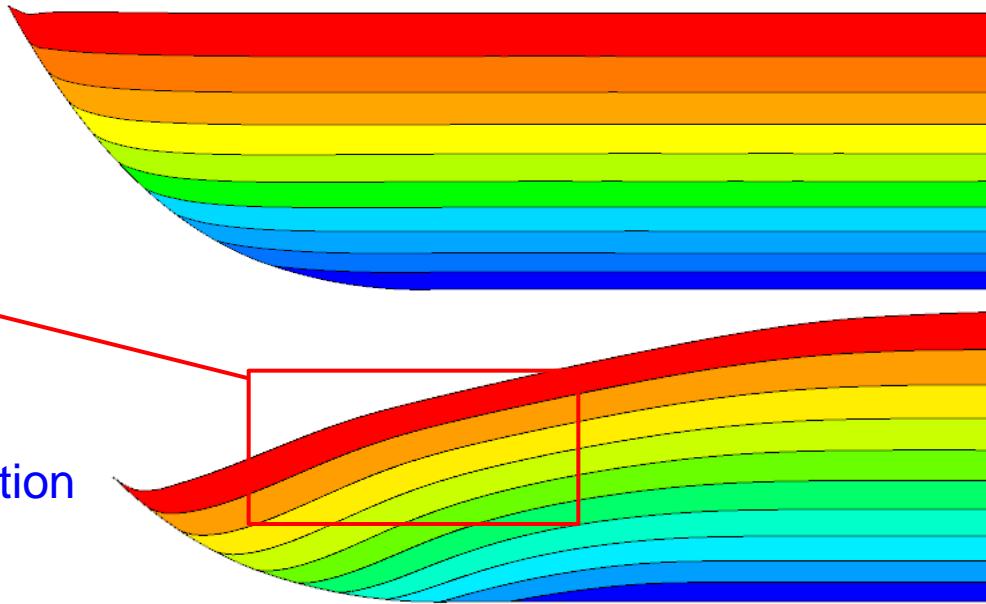
Collapse graben develops due to the increase in the bed lengths of the upper region of the pre-rift sand.



Shear in Field-Scale Diffuse Model

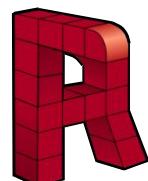
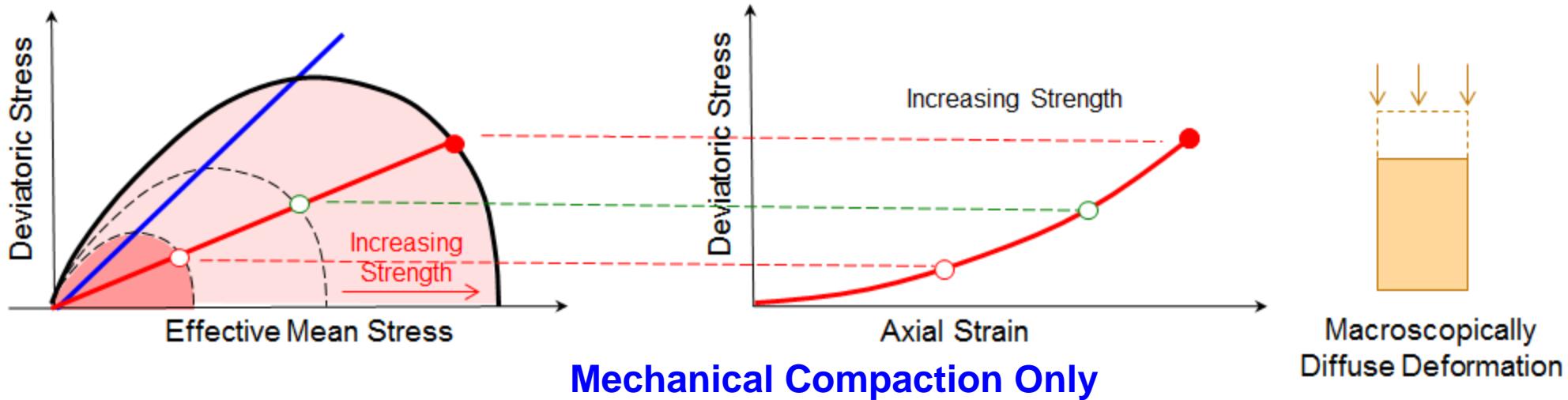


Field-scale Simulation including Deposition
(Mechanical Compaction Only)
Hydrostatic Pore Pressure



Regional-Scale Salt Tectonics Modelling

Critical State Based Model Uniaxial Compaction



Status and Further Work

- Good correlation between structural styles of experimental and numerical models as been observed..
- Better correlation can be achieved by improved calibration of numerical rheologies relative to experimental materials.
- Knowing more about the physical experimental set-up and design would allow for a more specific, rather than generic, comparison.
- Extension to the field-scale can be accommodated via consideration of rheological upscaling via thermal and chemical compaction processes.
- Parametric investigation of field scale processes and behaviour will be performed.

