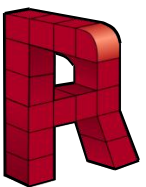
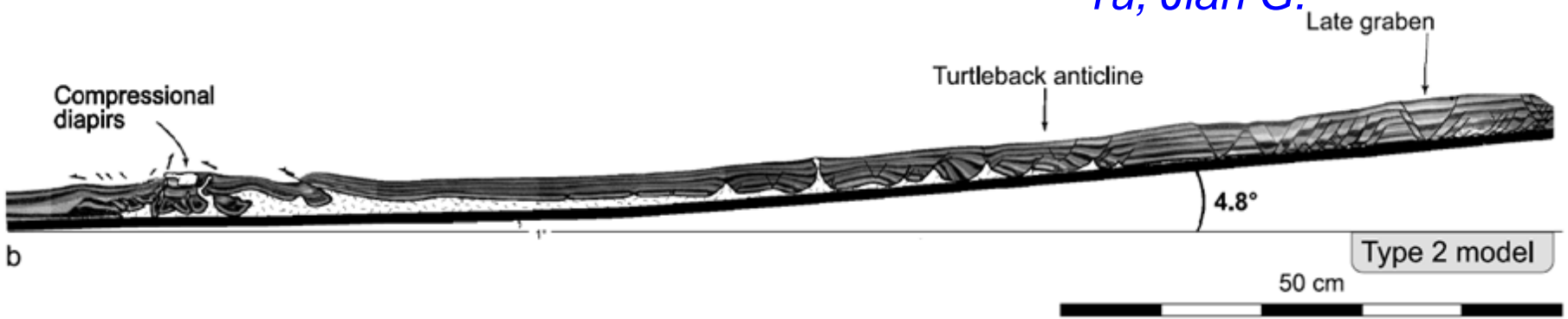


## Regional-Scale Salt Tectonics Modelling: Bench-Scale Validation and Extension to Field-Scale Predictions

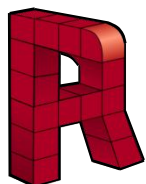
Thornton, Dean A.,  
Roberts, Daniel T.,  
Crook, Anthony J.L.,  
Yu, Jian G.



## ***Acknowledgements***

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- Special thanks to:
- European Social Fund (Kess Scholarship);
- Joe Cartwright – Seismic 3D Labs, Cardiff University
- Rockfield Software Ltd.

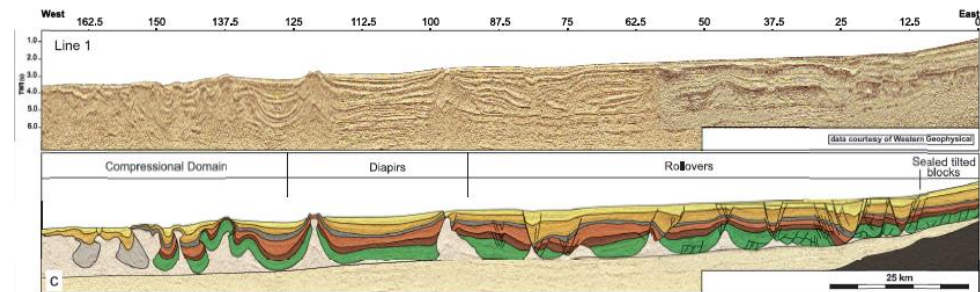


**Main Goal:** Determine main controls on structural styles and reservoir properties in a gravity driven system underlain by a mobile sub-strate

### Structural questions:

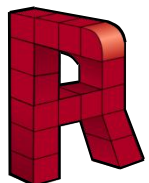
Major controls on structural style:

- timing of activity of structures (basement subsidence vs. sedimentary loading)
- spacing and style of extensional rafts
- transition to compressional regime
- influence of basement geometry



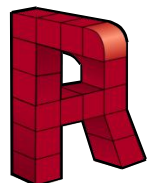
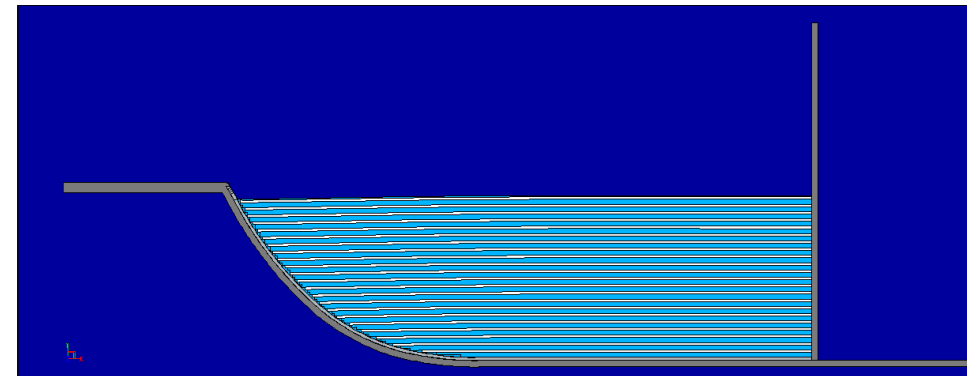
### Rationale

- Fort et al, 2004 performed laboratory experiments on brittle-ductile models to study thin-skinned deformation above the salt at margin scale
- The experiments are designed with the salt basin wedging out, both landward and seaward, and entirely covered by sediments at the onset of gravity driven deformation.
- They show that the experiments capture the main mechanisms observed in the seismic images

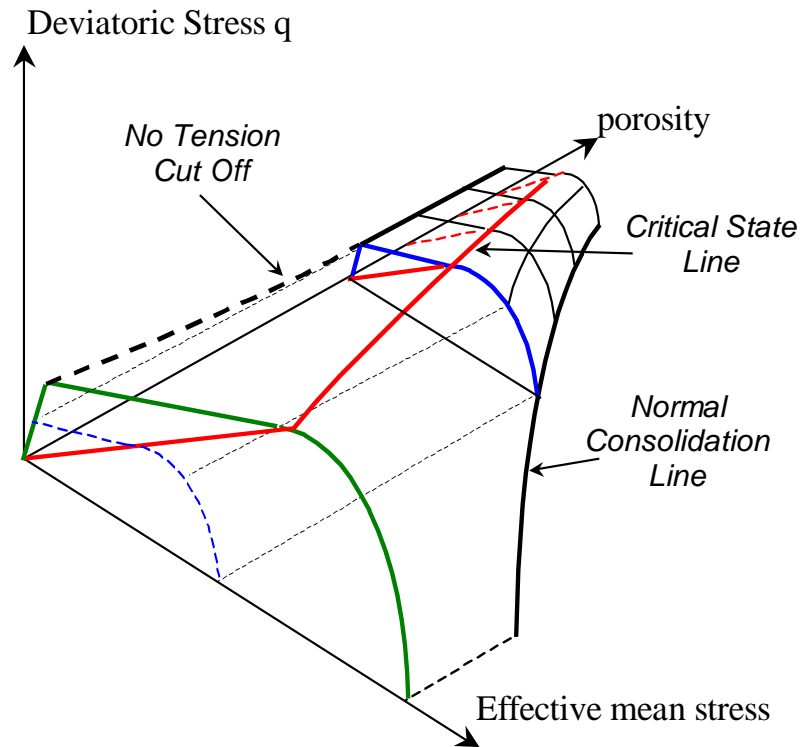


### ELFEN – Modelling Approach

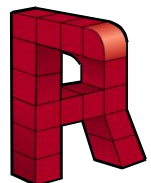
- **Finite Element Method**
- **Physics** based approach incorporating **large strain**
- Enhanced **rheological models** (constitutive models) for **rocks** and **salt**
- Enhanced **fault** and **localisation prediction**
- Includes **Sedimentation** and **Erosion**



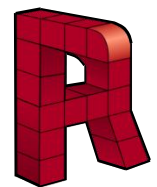
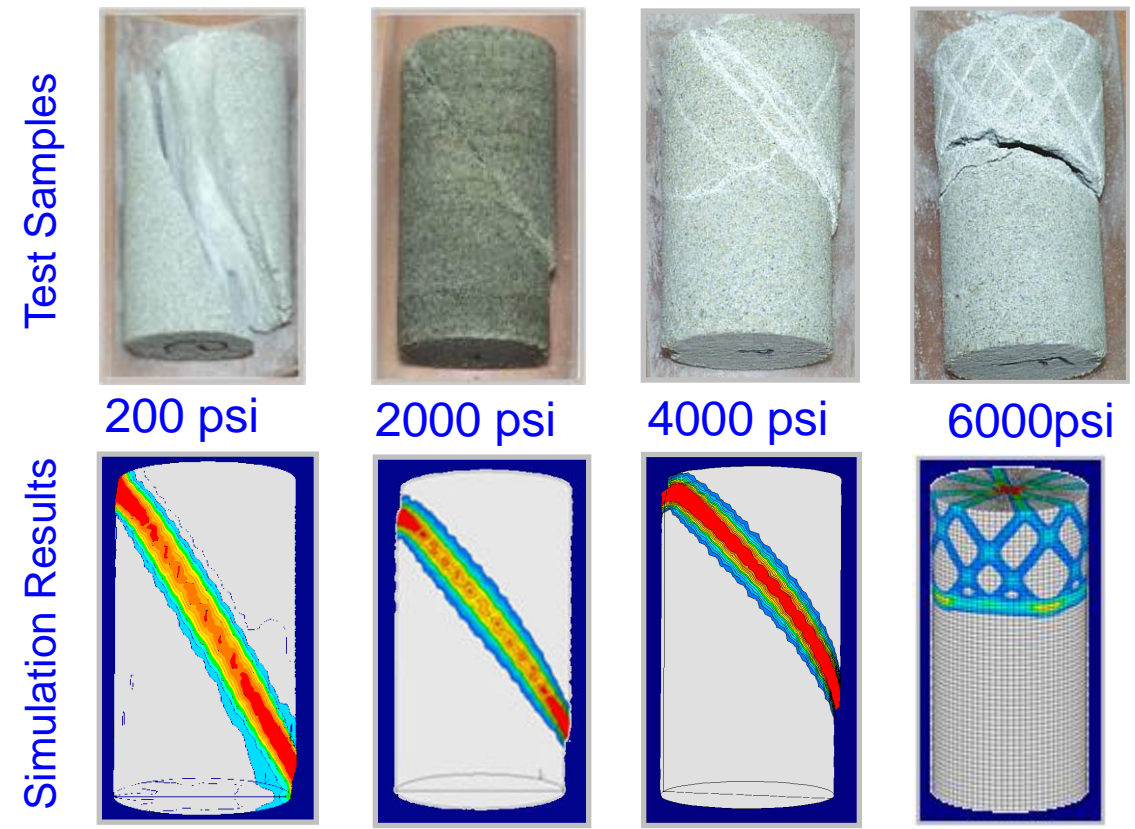
## Rockfield's SR3 Constitutive Model



- State Boundary Surface Based on **Critical State Theory**.
- Represents Increased strength due to **Mechanical Compaction** and Strength Reduction due to **Shear Failure**
- Fracture Mechanics Concepts facilitate scale-up from experimental to field scale
- Localisation Identification Algorithms enable the **prediction** of the **formation** and **evolution** of **new faults**



## Dependence of fracture angle on confining pressure



## SR3 Model - Characterisation

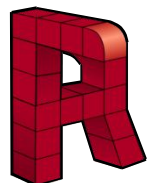
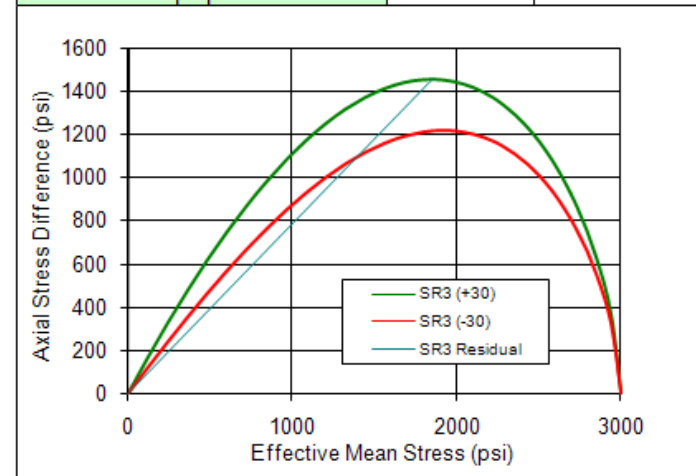
- The constitutive model has been shown to provide a good prediction of the response in sandbox tests in a number of different stress regimes.
- Elastic Properties:**  
Young's Modulus ( $E$ ) = 75,000 Pa  
Poisson's Ratio ( $\nu$ ) = 0.3
- Initial Porosity**  
 $\phi_0 = 0.45$
- SR3 Plasticity:**  
Residual Friction  $M = 0.79 \phi_{cs} = 20.34^\circ$

## Yield Surface Definition

### Soft Rock 3 Model

Yield Surface Definition Parameters	
Pre-Consolidation Pressure $p_c$	3000
Friction Parameter $\phi$ (°)	55.00
Tensile Intercept $p_t$	-1.00
Exponent $n$	1.6
Friction Parameter $\psi$ (°)	45.00
	0.785
Deviatoric Correction ( $\alpha$ )	0.25
Beta 0	0.6
Beta 1	3.00E-04

Residual Friction Angle $\phi_{cs}$	20.34
$Q_{cs}/p_{cs}$	0.79



## Herschel-Bulkley Model

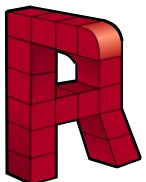
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- The silicone is represented using a Herschel-Bulkley material model. This relates the shear stress with the shear strain rate via

$$\tau = \tau_0 + k\dot{\gamma}^n$$

where  $\tau_0$  is the initial shear strength,  $k$  is the consistency parameter and  $n$  is an exponent.

- When  $\tau_0 \rightarrow 0$  and  $n = 1$  then this becomes a Newtonian fluid where the consistency parameter ( $k$ ) is the fluid viscosity ( $\mu$ )
- The silicon is defined as being Newtonian with  
 $\mu = 10000 \text{ Pa}\cdot\text{s}$  (2.778 Pa.hrs).
- This is achieved in ELFEN by setting  
 $\tau_0 = 0.2\text{Pa}$   
 $n = 1$   
 $k = 2.778 \text{ Pa}\cdot\text{hrs}$



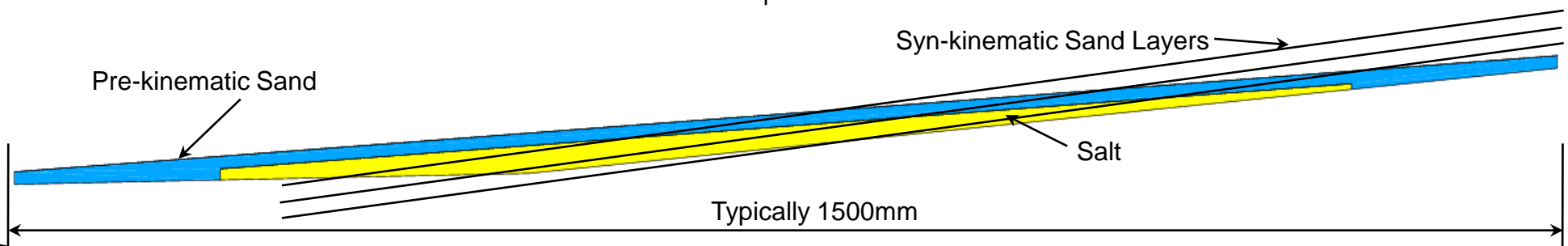


## Geometry

- Parametrically Defined to allow modification **slopes**, pre-kinematic sediment and salt thickness, **syn-kinematic layer thickness** and extent, sedimentation rate
- The **pre-kinematic layer is 5mm thick** in the extensional zone and may be either constant thickness or tapered towards the toe of the slope

## Loading and Boundary Conditions

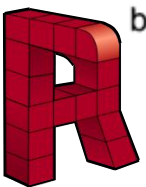
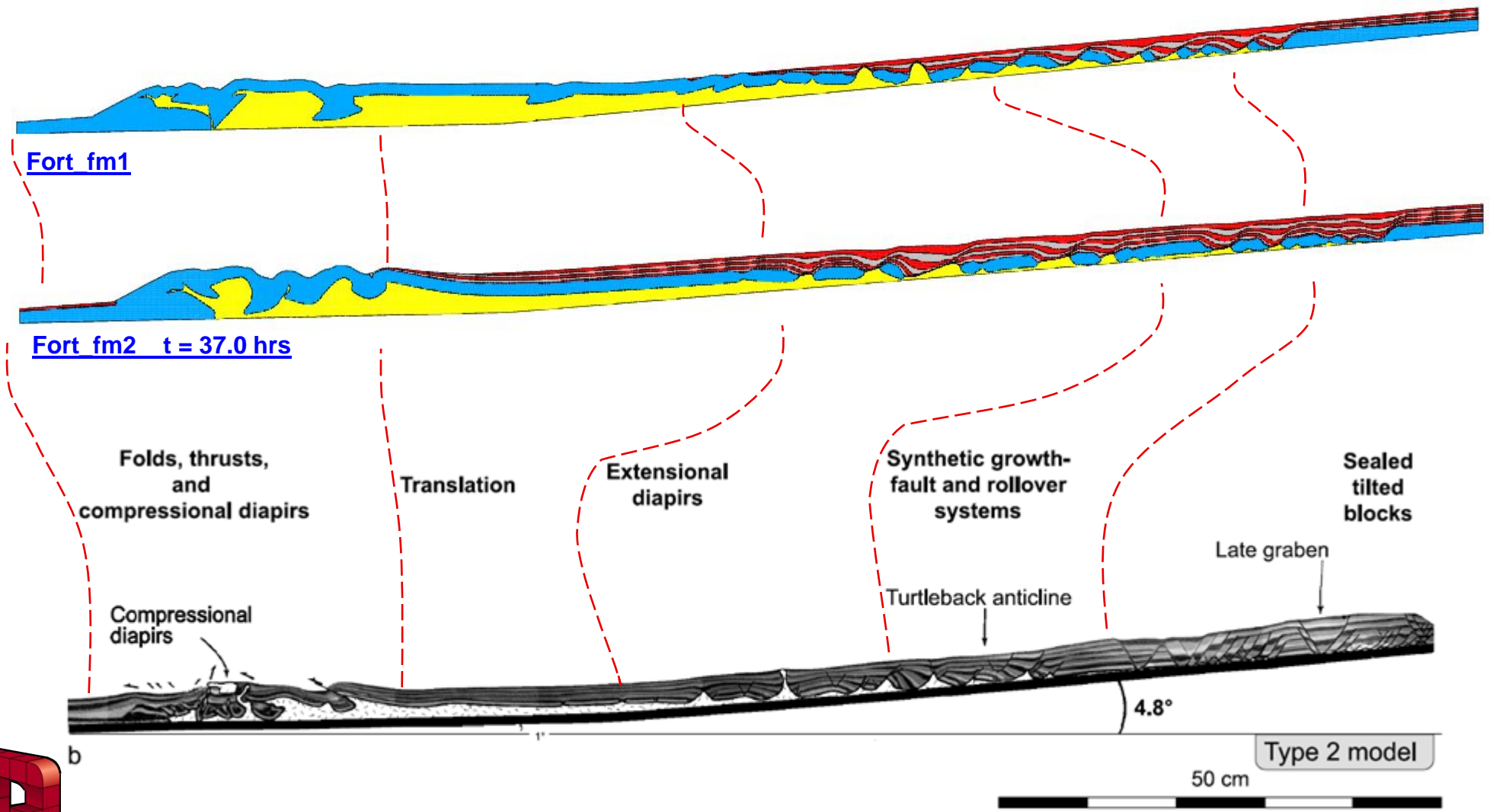
- Multi-stage analysis comprising
- Gravity initialisation of the salt and pre-kinematic sand
- Sedimentation of the syn-kinematic layers after a specified time (typically 5hrs)
- No slip at the sediment/sandbox and salt/sandbox interfaces.



# Regional-Scale Salt Tectonics Modelling

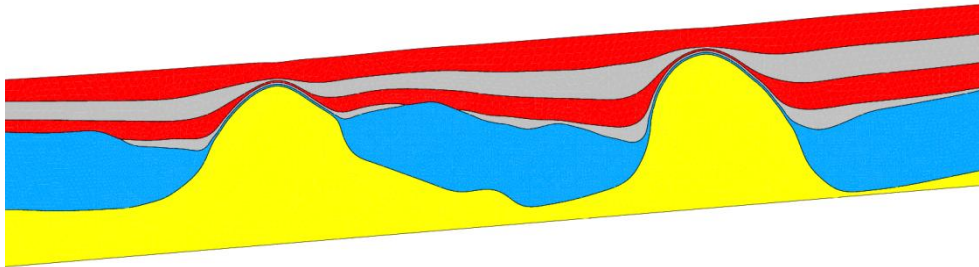
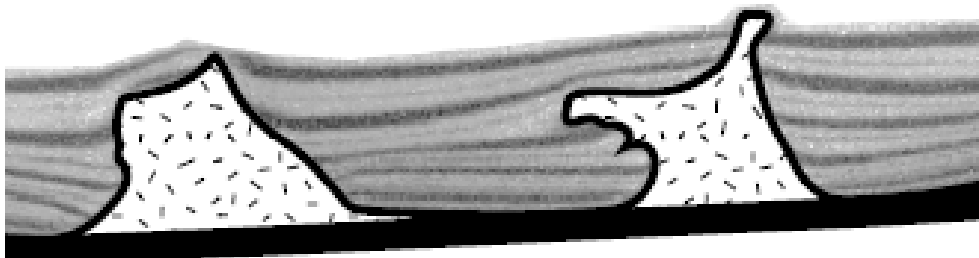
## Fort et al. (2004) Models

Fort\_fm1 - Distal slope angle 1°. Proximal slope angle 4.8°.  
Fort\_fm2 - Distal slope angle 1°. Proximal slope angle 3.8°.



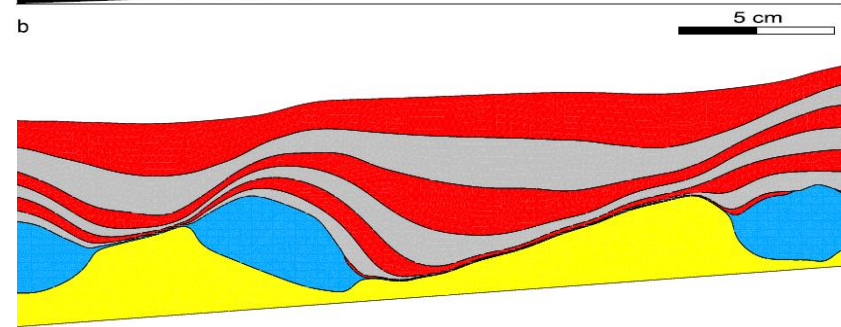
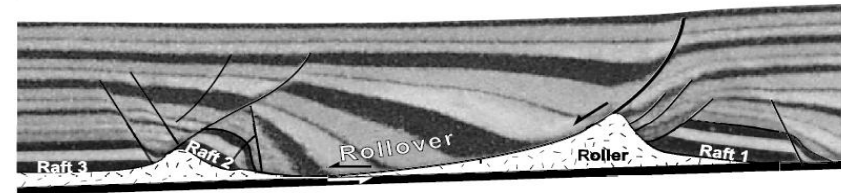
### Comparison of Structural Styles

Fort\_fm1

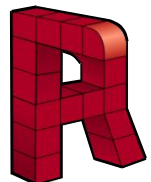


Diapirs in the proximal extension zone

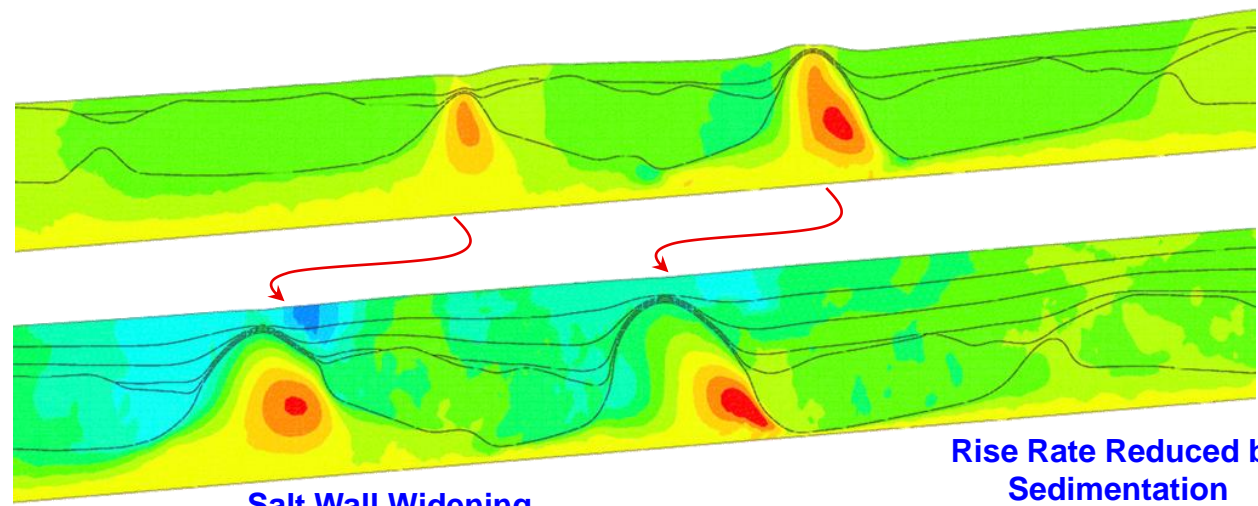
Fort\_fm2



Salt rollers in the proximal extension zone



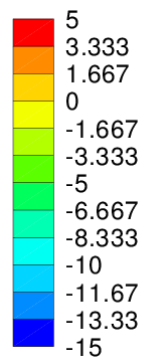
### Fort\_fm1



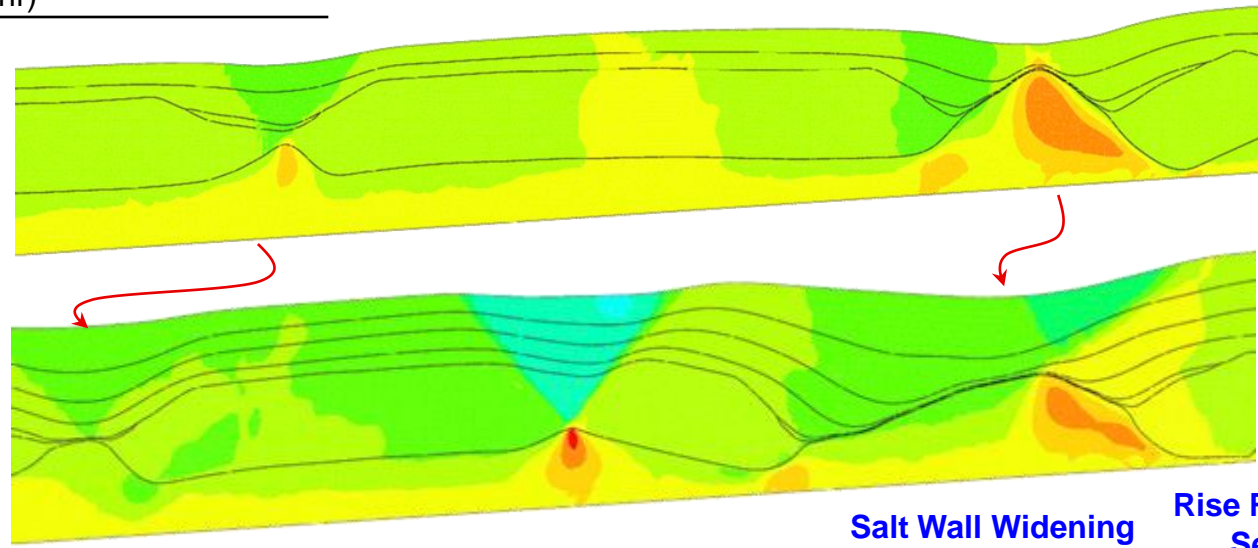
Vertical Velocity (mm/hr)

Salt Wall Widening

Rise Rate Reduced by Sedimentation



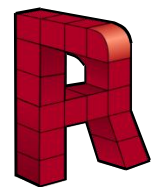
### Fort\_fm2



Vertical Velocity (mm/hr)

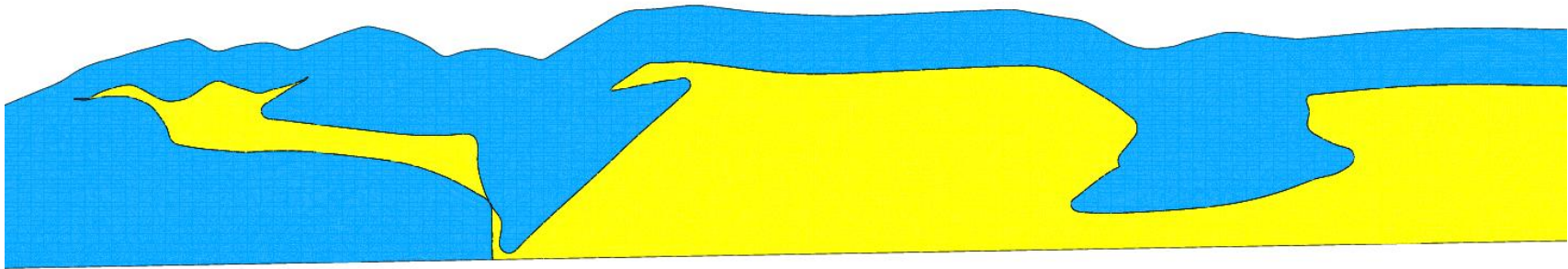
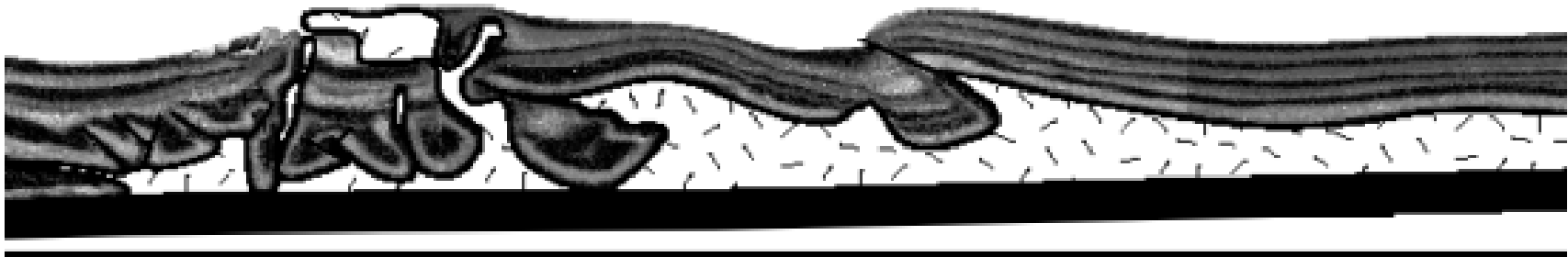
Salt Wall Widening

Rise Rate Reduced by Sedimentation



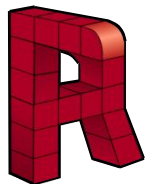


## Comparison of Structural Styles



Fort\_fm1

Enlarged view of compressional deformation in the physical and computational models

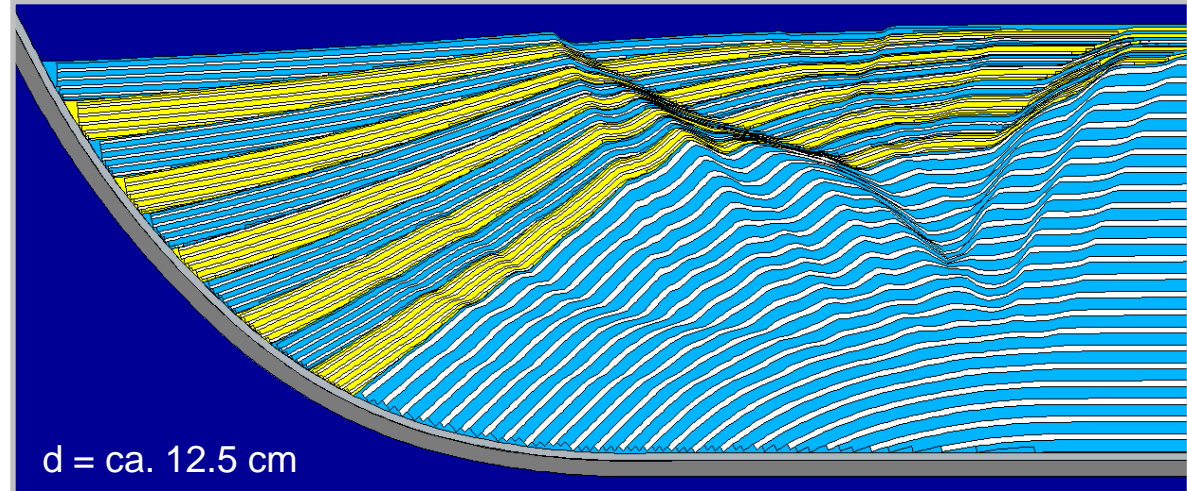




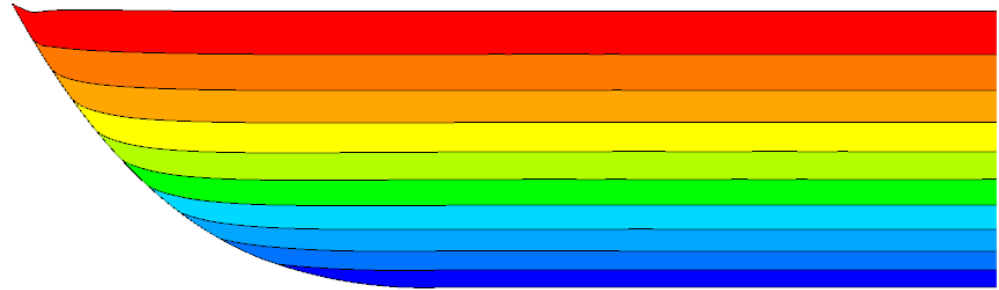
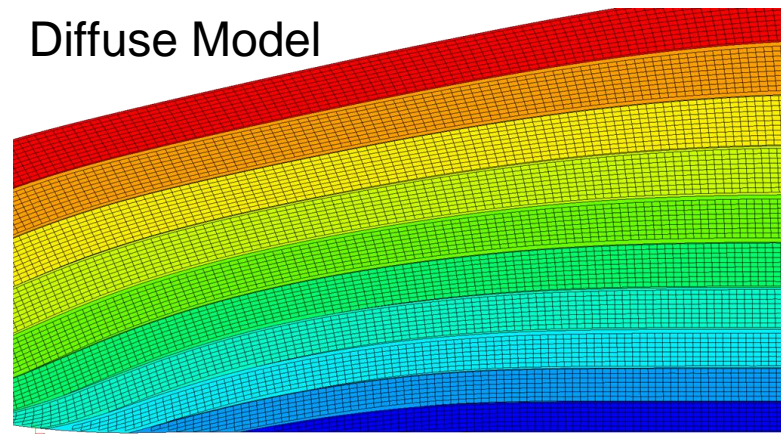
# Regional-Scale Salt Tectonics Modelling McClay E30/E37 Listric Fault Experiment and Prediction

## Bench-scale Simulation

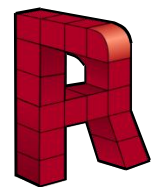
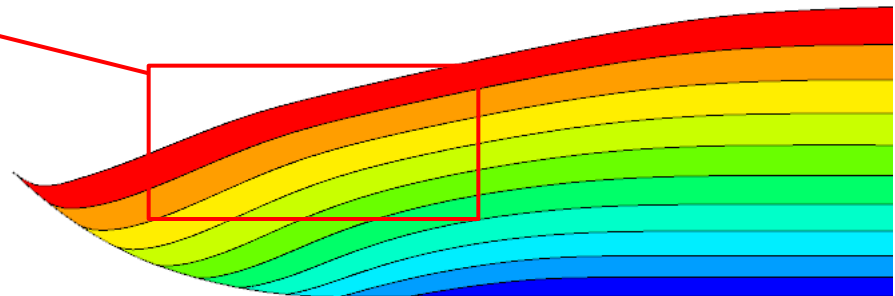
Collapse graben develops due to the increase in the bed lengths of the upper region of the pre-rift sand.



## Shear in Field-Scale Diffuse Model

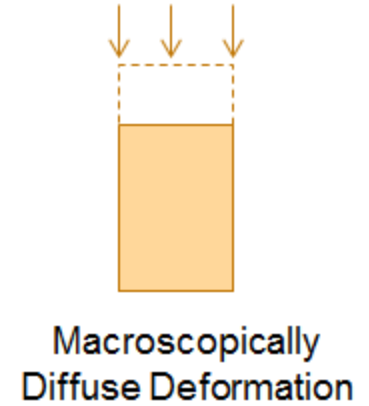
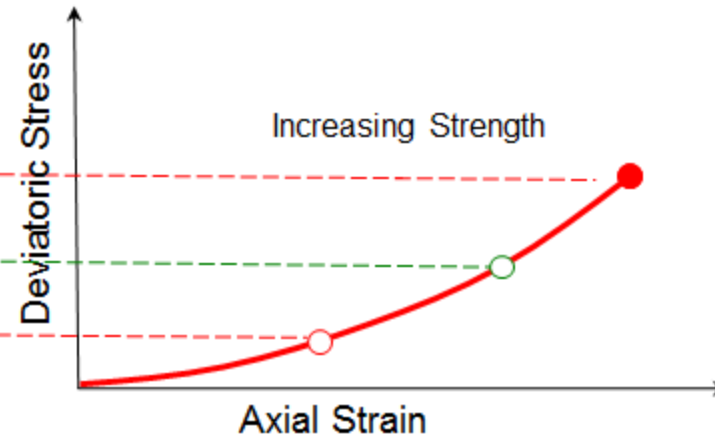
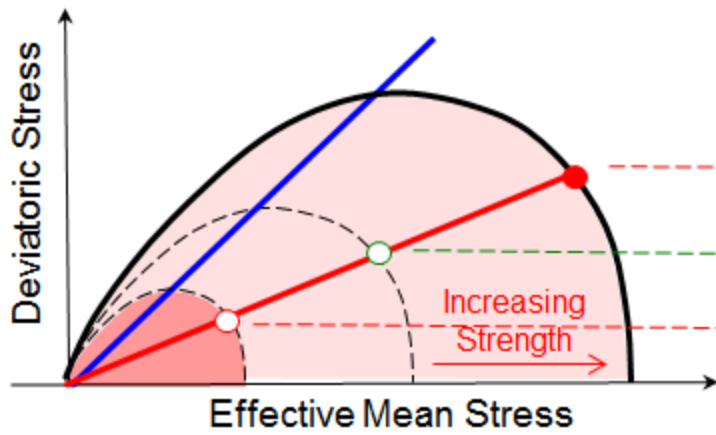


## Field-scale Simulation including Deposition (Mechanical Compaction Only) Hydrostatic Pore Pressure

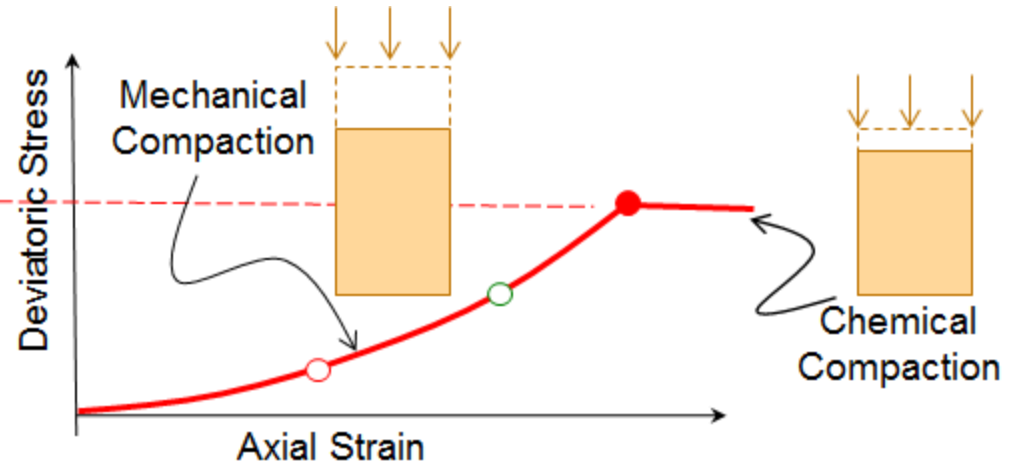
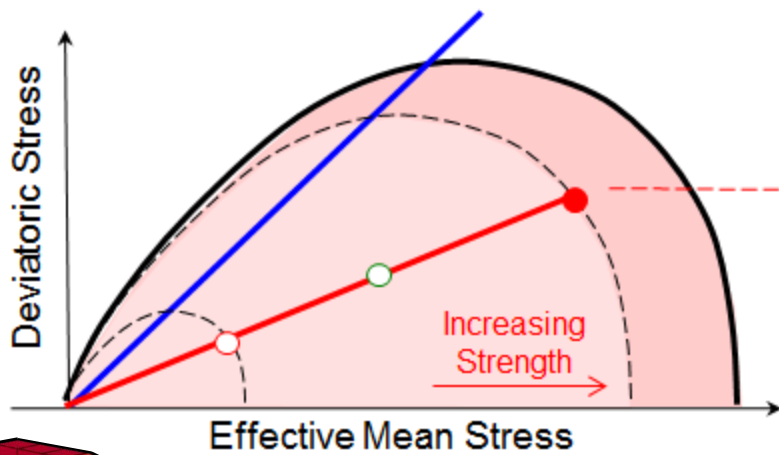


# Regional-Scale Salt Tectonics Modelling

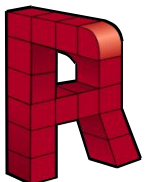
## Critical State Based Model Uniaxial Compaction



**Mechanical Compaction Only**



**Mechanical and Chemical Compaction**



### Status and Further Work

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- Good correlation between structural styles of experimental and numerical models as been observed..
- Better correlation can be achieved by improved calibration of numerical rheologies relative to experimental materials.
- Knowing more about the physical experimental set-up and design would allow for a more specific, rather than generic, comparison.
- Extension to the field-scale can be accommodated via consideration of rheological upscaling via thermal and chemical compaction processes.
- Parametric investigation of field scale processes and behaviour will be performed.

