



**T98. ENVIRONMENTAL AND ENGINEERING GEOLOGY STUDENT RESEARCH COMPETITION** 

## Seawater Intrusion Effect on Radioactive Strontium Mobility

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- 01. Background
- 02. Research Approach
- **03. Materials and Method**
- 04. Results
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- Pure  $\beta$ -emitter,  $T_{1/2} = 28.8$  y
- <sup>90</sup> Sr migration is controlled by sorption reactions (i.e., ion-exchange).
- In general, <sup>90</sup>Sr sorbs on clay / Fe-oxides / other minerals
   → via weakly bound outer-sphere surface complexes
- Degree of sorption
  - : depends on factors (e.g. pH / I.S./ solid phase composition/ surface area)



Dan Hawkes, U.S. Department of Energy, 2013



J. P. Mckinley, et. al., 2007







## 2. Salinization and <sup>90</sup>Sr leak scenarios at a NPP site



#### <Objectives>

- To determine  $K_d$  and R depending on different ionic strength degrees in solution
- To model quantitatively the amount of sorption affinity of <sup>90</sup>Sr as a function of the corresponding activities in solution
- To compare the exchange convention for describing the data set





## 3.1. Materials

- Study area : Shin-Gori 3-4 reactor site in Koera
- Solid samples : core rock (shattered zone), GL(-) 6.6 7.4 m



< Mineral composition, % >			
Quartz	22.20		
Albite	39.00		
Orthoclase	19.00		
Muscovite	6.00		
Biotite	3.00		
Chlorite	6.00		
Actinolite	4.80		
Total	100.00		



Cation exchange capacity

	Solution	samp	les
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Methods	Fraction size	CEC [µeq/g]
NH <sub>4</sub> -OA <sub>c</sub> (pH 7)	0.5 – 1 mm	23.11
1 M of NaNO <sub>3</sub> / KNO <sub>3</sub> (pH 7)	< 2 mm	24.21

	рН	I.S. [M]
GW	7.70	0.005
SW	8.08	0.770





## 3.2. Batch & Column exp.

#### <Batch adsorption>

- < 1 mm size solid, adsorbent (0.5 g/ 10 mL)</p>
- <sup>90</sup>Sr 10 Bq/mL, reaction time 10 d
- Experimental procedure
   initial concentration : <sup>90</sup>Sr 10 Bq/mL





#### <Column>

- 0.5 1 mm fractionated solid
- Stable Sr (ICP-OES analysis)
- Injected Br / Sr: 10071 and 0.175 mg/L
- Column set-up condition

No.	Type fluids	I.S. [M]	Porosity (θ)	Bulk density [g/cm <sup>3</sup> ]	Pore vol. [cm <sup>3</sup> ]	Flow rate [mL/min]
1	GW	0.005	0.42	1.43	11.73	
2	GW+SW (50 : 50)	0.388	0.40	1.55	11.00	0.03
3	SW	0.770	0.41	1.49	11.33	





## 3.3. Binary ion-exchange exp.

- 75 150 µm fractionated solid (non pretreated)
- Reaction time: 12 h (0.5 g /10 mL)
- Initial pH of solutions: pH 7
- Chemical reagent: NaNO<sub>3</sub>, KNO<sub>3</sub>, Ca(NO<sub>3</sub>)<sub>2</sub>·4H<sub>2</sub>O, and Mg(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O



• Experimental procedure







- Selectivity coefficient, K<sub>selectivity</sub>
  - indicate the adsorption affinity to the solid materials
    - : dependence on pH, I.S., sorbent heterogeneity, specific adsorption, or variation of the activity of the adsorbed species
  - Mole fraction

 $x_{Sr} = q_{Sr} / (qSr + qM)$ 

Equivalent fraction

 $y_{Sr} = q_{Sr} / (2qSr + qA)$  $y_{Sr} = q_{Sr} / (2qSr + 2qB)$ 

M: competing cation (Na<sup>+</sup>, K<sup>+</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup>) A: monovalent cation (Na<sup>+</sup>, K<sup>+</sup>) B: divalent cation (Ca<sup>2+</sup>, Mg<sup>2+</sup>) q: amount of bound cations a: activities in solution SrX, AX and BX: exchanger phase with -1 charge SrY, AY and BY: exchanger phase with -2 charge

$$SrX_2 + 2A^+ = A_2X_2 + Sr^2^+$$

V(surface site) = -1'

 $SrX_2 + B^{2^+} = BX_2 + Sr^{2^+}$ 

<hetero-exchange> <homo-exchange>

$$K_{Vanselow} = \frac{a_{sr} x^2 A}{a^2 A x_{sr}} \text{ or } = \frac{a_{sr} x B}{a B x S r}$$
$$K_{Gaines \_Thomas} = \frac{a_{sr} y^2 A}{a^2 A y_{sr}} \text{ or } = \frac{a_{sr} y B}{a B y_{sr}}$$

• Y(surface site) = `-2`  $SrY + 2A^+ = A_2Y + Sr^2^+$  <hetero-exchange>  $SrX_2 + B^{2^+} = By + Sr^{2^+}$  <homo-exchange>

$$K_{Cernik} = \frac{a_{Sr}yA}{a^2A y_{Sr}}$$
 or  $= \frac{a_{Sr}yB}{aB y_{Sr}}$ 





## 3.4. Salinity effect on exchangeable Sr

- 75 150 µm fractionated solid (non pretreated)
- original GW and SW
- 0.5 g / 10 mL<sup>-1</sup>
- Reaction time: 1, 4, 12 h and 1, 3, 7, 14, 30 d
- Solution types

Name	GW : SW [%]	I.S. [M]	рН	Sr [mg/L]
SET 1	100 : 0	0.01	7.81	0.23
SET 2	70 : 30	0.24	7.90	2.09
SET 3	50 : 50	0.39	8.00	3.33
SET 4	30 : 70	0.54	8.01	4.65
SET 5	0 : 100	0.77	8.10	6.50





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## 4.1. Batch & Column experimental Results

#### <Results of batch adsorption>

•	Sorption	distribution	coefficient	$(\mathbf{K}_d)$	of	<sup>90</sup> Sr
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No.	Fluid type	I.S. [M]	рН	<i>K<sub>d</sub></i> [mL/g]
1	GW	0.005	7.81	39.0
2	GW+SW (50 : 50)	0.388	8.00	26.2
3	SW	0.770	8.10	13.4

#### <Results of column – Br tracer>

Dispersion coefficient (D) from CXTFIT equilibrium model fit

No.	Fluid type	I.S. [M]	R	D [cm²/min]
1	GW	0.005	1	0.01
2	GW+SW (50 : 50)	0.389	1	0.01
3	SW	0.770	1	0.02







#### <Results of Sr transport>







## 4.2. Binary ion-exchange exp.

• Sr<sub>Solid</sub> - Na<sup>+</sup>

log I.S. [M]	log Sr <sub>extracted</sub> [M]	log K <sub>G-T</sub>
-3.6	-7.87	3.59
-2.7	-7.38	2.65
0.2	-6.16	1.60

Sr<sub>Solid</sub> - K<sup>+</sup>

log I.S. [M]	log Sr <sub>extracted</sub> [M]	log <i>К</i> <sub>G-т</sub>
-4.7	-7.66	3.89
-3.3	-6.86	3.08
-0.3	-6.42	0.13

■ Sr<sub>Solid</sub> – Ca<sup>2+</sup>

log I.S. [M]	log Sr <sub>extracted</sub> [M]	<b>К</b> <sub>G-T</sub>
-4.7	-7.87	1.00
-2.7	-6.37	0.99
0.2	-6.59	0.84

log I.S. [M]	log Sr <sub>extracted</sub> [M]	log <i>К</i> <sub>G-T</sub>
-4.1	-7.68	0.99
-2.1	-6.09	0.97
0.9	-6.86	0.52







#### <hetero-exchange isotherm>

Sr<sub>Solid</sub> - Na<sup>+</sup>

log I.S. [M]	log Sr <sub>extracted</sub> [M]	log K <sub>Vanselow</sub>	log К <sub>G-T</sub>	log K <sub>Cernik</sub>
-3.6	-7.87	3.89	3.59	3.58
-2.7	-7.38	2.95	2.65	2.64
0.2	-6.16	1.90	1.60	1.60

Sr<sub>solid</sub> - K<sup>+</sup>

log I.S. [M]	log Sr <sub>extracted</sub> [M]	log K <sub>Vanselow</sub>	log К <sub>G-T</sub>	log <i>K</i> <sub>Cernik</sub>
-4.7	-7.66	4.19	3.89	3.89
-3.3	-6.86	3.38	3.08	3.08
-0.3	-6.42	0.43	0.13	0.13







#### <homo-exchange isotherm>

■ Sr<sub>Solid</sub> – Ca2+

log I.S. [M]	log Sr <sub>extracted</sub> [M]	Kvanselow	<b>К</b> <sub>G-T</sub>	<b>K</b> Cernik
-4.7	-7.87	1.00	1.00	1.00
-2.7	-6.37	0.99	0.99	0.99
0.2	-6.59	0.84	0.84	0.84

Sr<sub>Solid</sub> – Mg2<sup>+</sup>

log I.S. [M]	log Sr <sub>extracted</sub> [M]	<b>K</b> <sub>Vanselow</sub>	К <sub>G-T</sub>	<b>K</b> <sub>Cernik</sub>
-4.1	-7.68	0.99	0.99	0.99
-2.1	-6.09	0.97	0.97	0.97
0.9	-6.86	0.52	0.52	0.52







## 4.3. Salinity effect on exchangeable Sr

Sr removal efficiencies	Name	GW : SW [%]	I.S. [M]	Sr <sub>initial</sub> [mg/L]	Sr <sub>after reaction</sub> [mg/L]	Max. Sr <sub>solution</sub> removal [%]
in solution	SET 1	100 : 0	0.01	0.23	0.14	39.5
	SET 2	70 : 30	0.24	2.08	1.91	8.18
	SET 3	50 : 50	0.39	3.33	3.06	8.11
	SET 4	30 : 70	0.54	4.65	4.02	13.7
	SET 5	0 : 100	0.77	6.49	5.52	15.0
50 40 8		•	<ul> <li><set 1=""> GW:</set></li> <li><set 2=""> GW:</set></li> <li><set 3=""> GW:</set></li> <li><set 4=""> GW:</set></li> <li><set 5=""> GW:</set></li> </ul>	5W = 100:0 5W = 70:30 5W = 50:50 5W = 30:70 5W = 0:100		
20 20 20						
10		•		•		
0 6	12	18	24	30	1	
R	eaction ti	ime [d]				





## 4.3. Salinity effect by kinetic reaction

 Sr removal efficiencies in solution



Name	GW : SW [%]	I.S. [M]	Sr <sub>solution</sub> removal [%]
SET 1	100 : 0	0.01	39.5
SET 2	70 : 30	0.24	8.18
SET 3	50 : 50	0.39	8.11
SET 4	30 : 70	0.54	13.7
SET 5	0 : 100	0.77	15.0

→ Precipitation as 'Strontianite'  $Sr^{2+} + HCO^{3-} \rightarrow SrCO_3(s) \downarrow + H^+$ (log Q/K = 1.3010 s/sat)





## **5.** Conclusions

- Sr sorption distribution coefficient ( $K_d$ ) decreased by increasing I.S.
  - : Sr sorption affinity in groundwater decreased with the seawater intrusion
- The mobility of Sr decreased in groundwater column

   higher Sr sorption affinity in groundwater condition than seawater
   due to low amounts of competing cations.
- Sr-Na exchange showed linear isotherm
   Sr ion-exchange reaction affected by divalent cations at low I.S. condition, however, Na<sup>+</sup> ion should be more affected factor at high I.S. condition.
- Vanselow and Gains-Thomas conventions well described Sr hetero-exchange reaction, while Gains-Thomas showed better homo-exchange isotherm under low I.S. condition.
- Strontianite precipitation occurs at high concentration of Sr in seawater solution.

**<Future study>** The additional model parameters have to be optimized to improve the model fit and to handle the variability of  $K_{selectivity}$  for Sr transport model.







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# **Thanks for your attention!**

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